

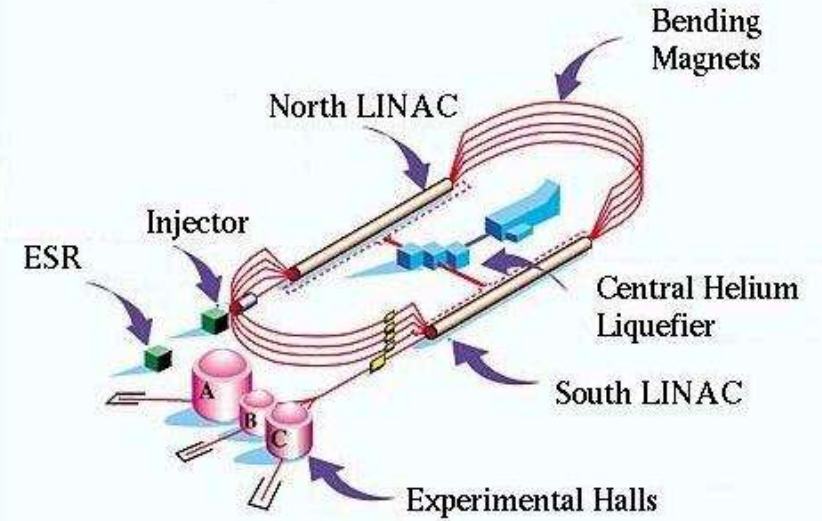
Development of a Frozen Spin Target for CLAS

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Target Group
Jefferson Lab

June 4, 2005
Miltenberg



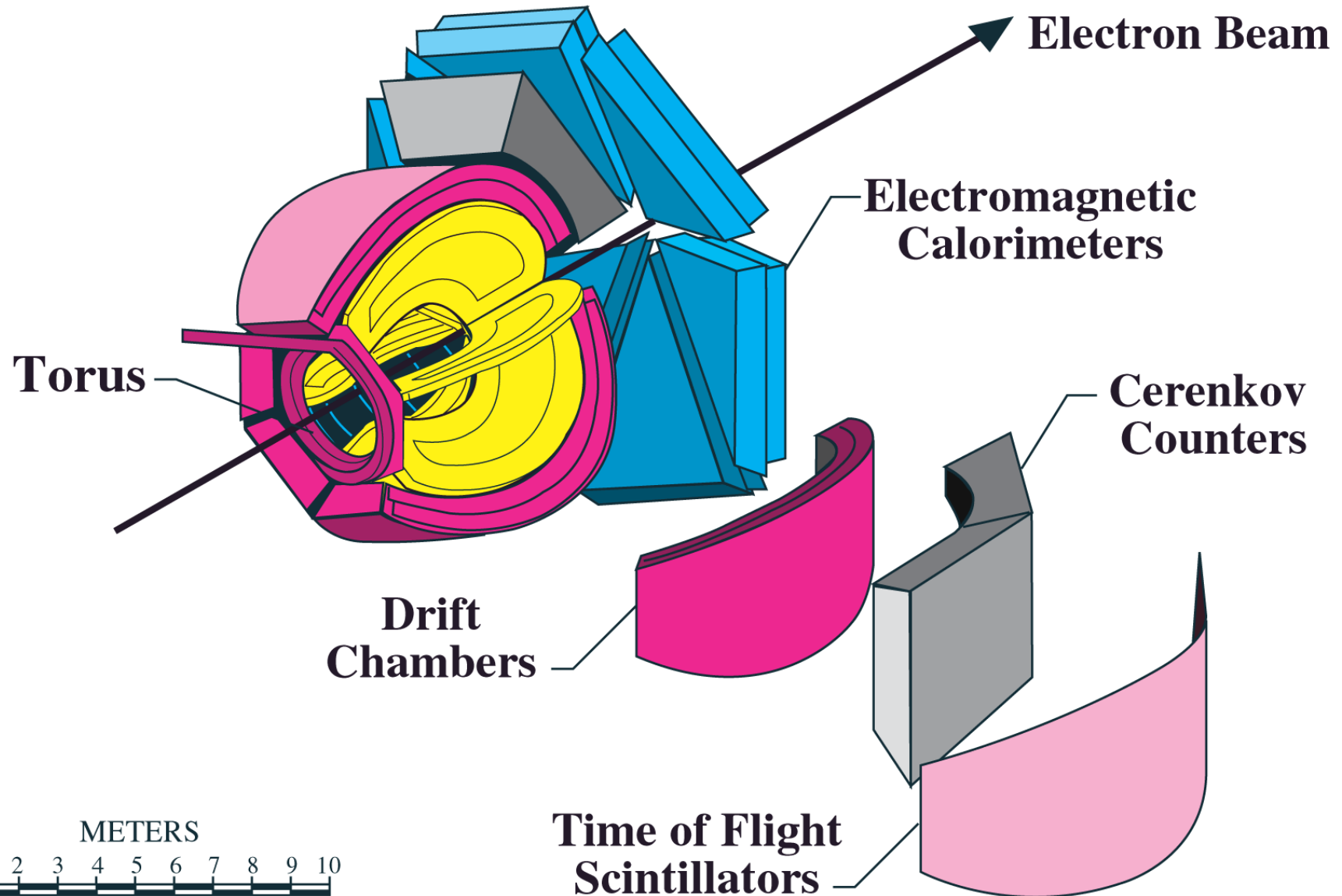
CEBAF – Continuous Electron Beam Accelerator Facility



Jefferson Lab Milestones

- 1976 CEBAF proposed
- 1983 DOE awards contract to SURA
- 1987 Groundbreaking for accelerator
- 1993 1st Experiments commence
- 1996 Name changed to Th. Jefferson Nat'l Accelerator Facility
- 1997 5-pass beam (4 GeV) simultaneously delivered to all 3 Halls
- 2000 6 GeV enhanced design goal met

LARGE ACCEPTANCE SPECTROMETER



The Conventional Hall B Polarized Target

Protons (and deuterons) in $^{15}\text{NH}_3$ ($^{15}\text{ND}_3$) are **continuously** polarized by 140 GHz microwaves at 5 Tesla, 1 Kelvin

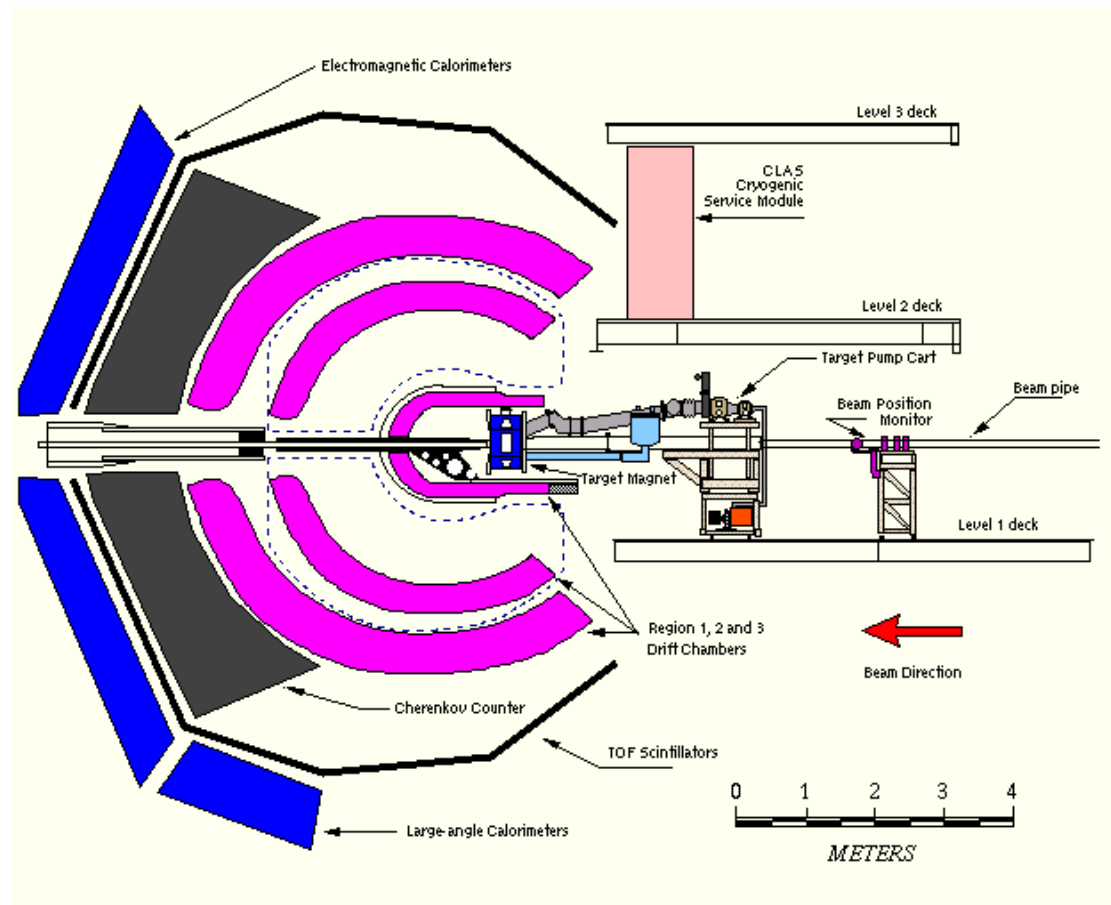
Used for several experiments (beam current ~ 3 nA) over a 10 month period during 1999, and 2000-2001

Proton polarization: $\sim 75 - 85\%$

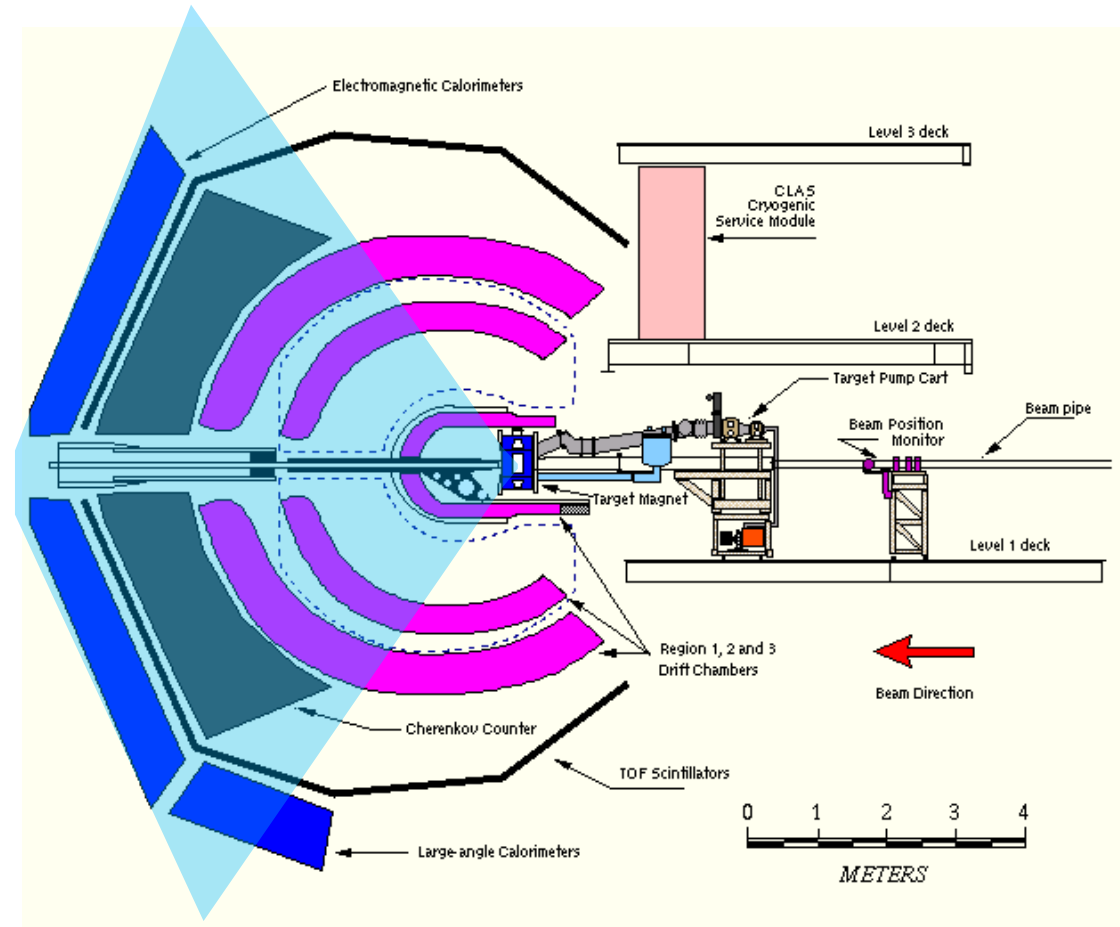
Deuteron polarization: $\sim 25 - 35\%$



The Current Hall B Polarized Target



The Current Hall B Polarized Target



Problem:

We have a “ 4π ” detector. We need a “ 4π ” target!

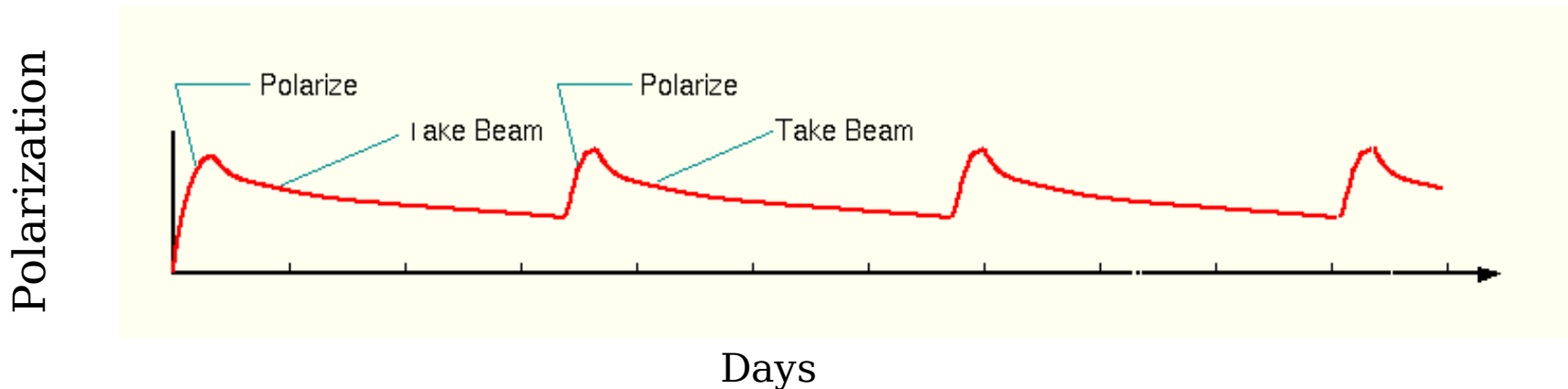
Frozen Spin Polarized Targets

Two steps

1. Polarize target material (NH_3 , $\text{C}_4\text{H}_9\text{OH}$, ${}^6\text{LiD}$, ...) at high field (2.5 – 5.0 T) and moderate temperature (.2 - .4 K)
2. Reduce target temperature to ~ 50 mK, and hold polarization with reduced field (0.3 – 0.5 T)

The target polarization then decays exponentially during the data acquisition phase of the experiment.

The target must be re-polarized (step 1) every few days.



Specifications for the Hall B Frozen Spin Target

Beam: Tagged photons

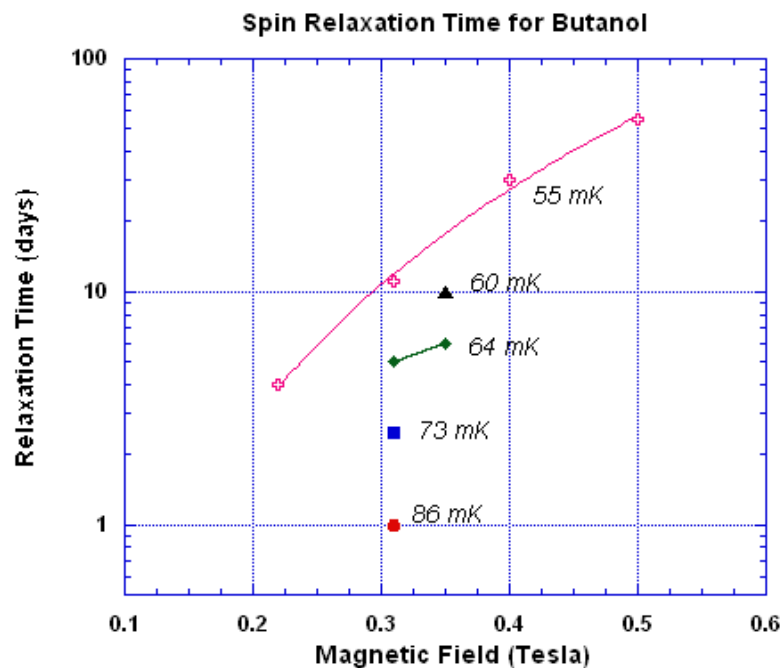
Target: $\text{Ø}15 \text{ mm} \times 50 \text{ mm}$ butanol ($\text{C}_4\text{H}_9\text{OH}$) $\mathcal{L} \sim 10^{30} - 10^{31}/\text{s cm}^2$

Polarizing Magnet: 5 Tesla warm bore solenoid

Holding Magnet: 0.3 – 0.5 Tesla internal solenoid

Refrigerator: $^3\text{He}/^4\text{He}$ dilution 'fridge $Q \sim 20 \text{ mW @ } 0.3 \text{ K}$

$Q \sim 10 \mu\text{W @ } 0.05 \text{ K}$



Ch. Bradtke

PhD Thesis, Univ. Bonn, 1999

Physics Program with Polarized Target and Tagged Photons

Approved Experiments

E02-112: Missing Resonance Search in Hyperon Photoproduction

E01-104: Helicity Structure of Pion Photoproduction

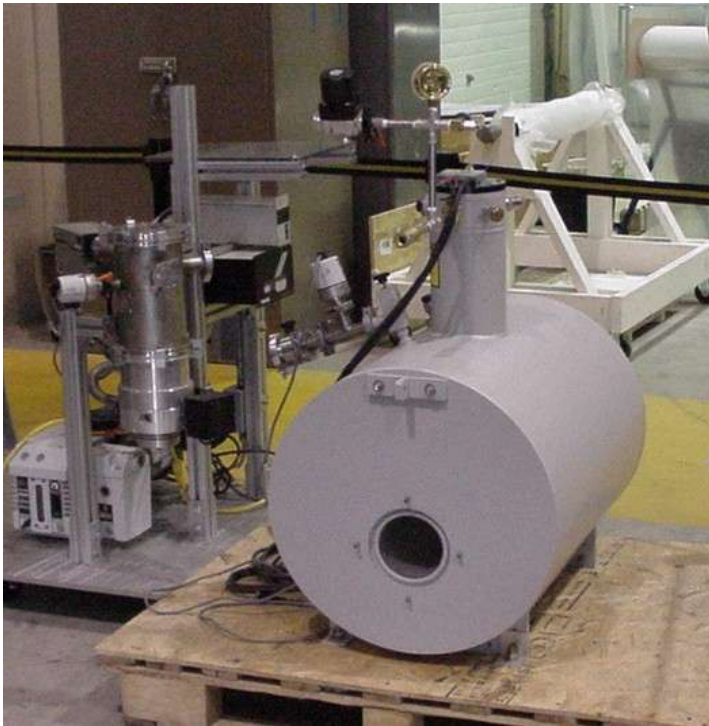
E03-105: Pion Photoproduction from a Polarized Target

Letter of Intent

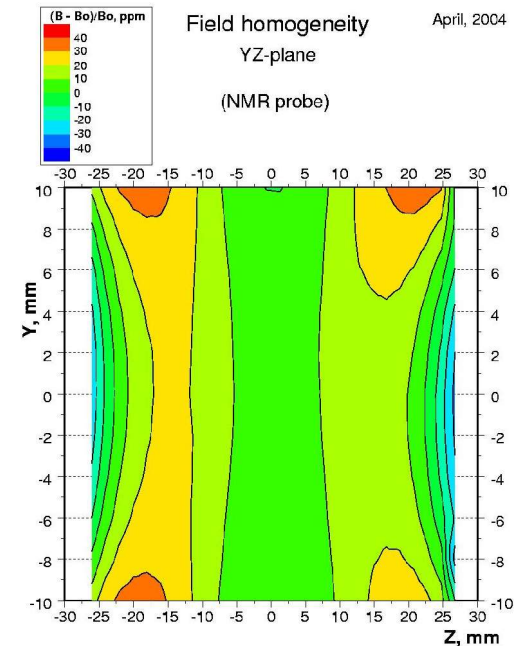
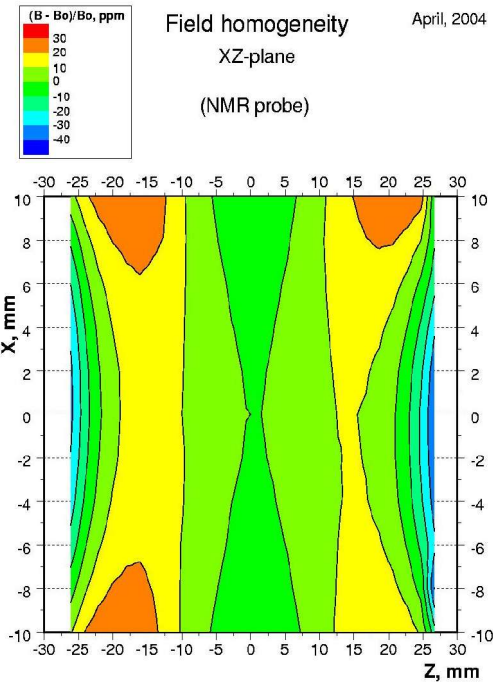
LOI-020104: Photoproduction Using Polarized Beam and Target

Polarizing Magnet

Max. Field: 5.1 T
 $\Delta B/B: < 3 \times 10^{-5}$
Bore: $\text{Ø}127 \text{ mm}$



Cryomagnetics, Inc.
Oak Ridge, TN, USA



A. Dzyubak, priv. comm..

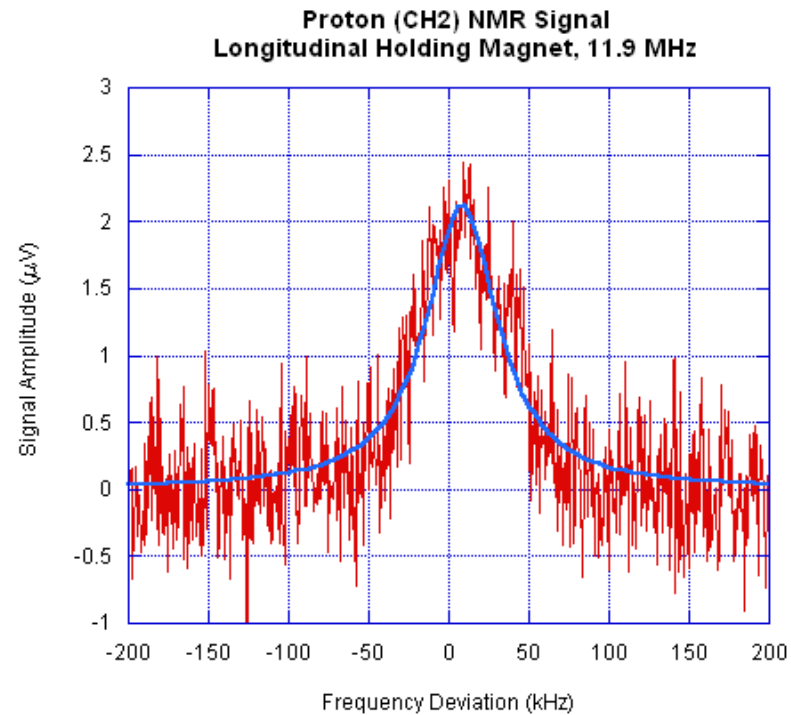
Holding Magnet, Longitudinal

Wire: \varnothing .1 mm multifilament NbTi, three layers

Dimensions: \varnothing 50 \times 110

Max. Field: 0.42 Tesla

Homogeneity: $\Delta B/B \sim 3 \cdot 10^{-3}$



Holding Magnet, Transverse (Prototype)

Wire: $\text{\O}1$ mm multifilament NbTi, three layers

Dimensions: $\text{\O} 40 \times 355$ mm

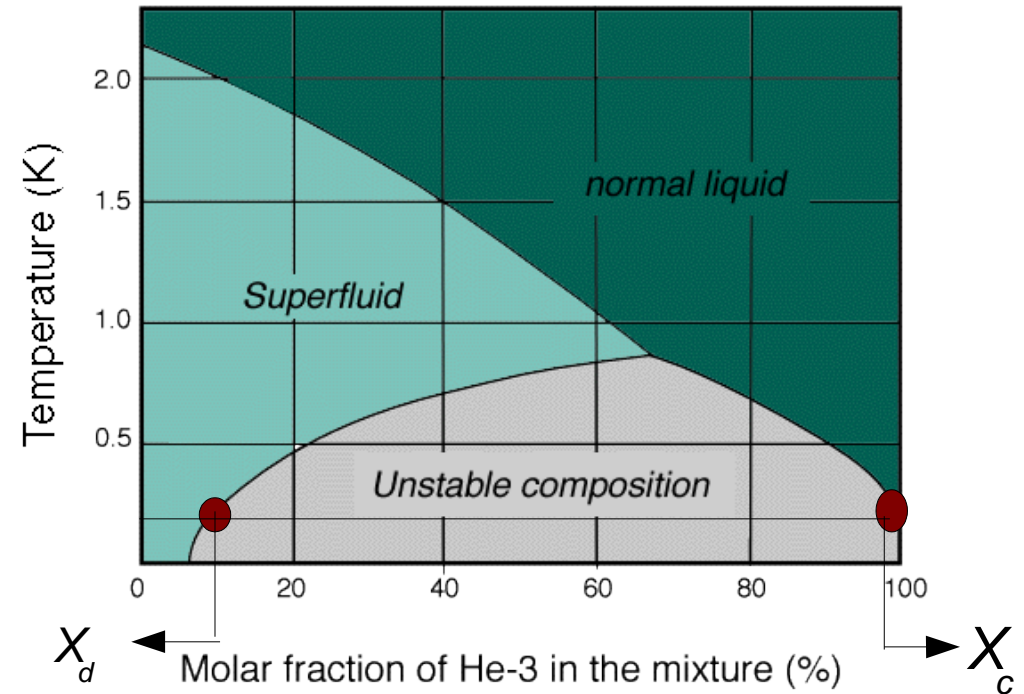
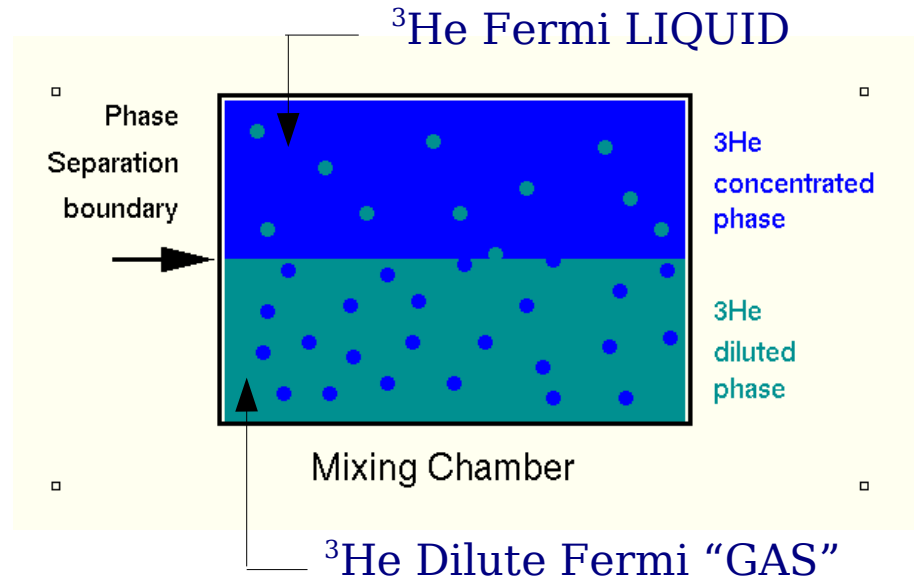
Max. Field: 0.27 Tesla

Homogeneity: $\Delta B/B \sim 5 \cdot 10^{-3}$



$^3\text{He}/^4\text{He}$ Dilution Refrigeration

- below 0.8 K, a $^3\text{He}/^4\text{He}$ mixture will separate into two phases



- if ^3He atoms are removed (distilled) from lower phase ^3He atoms from upper phase will cross the phase boundary to reestablish equilibrium

- ^3He will absorb energy when it dissolves into the dilute phase.

- heat absorbed by n moles is:

$$Q = n [H_d(T_m) - H_c(T_m)]$$

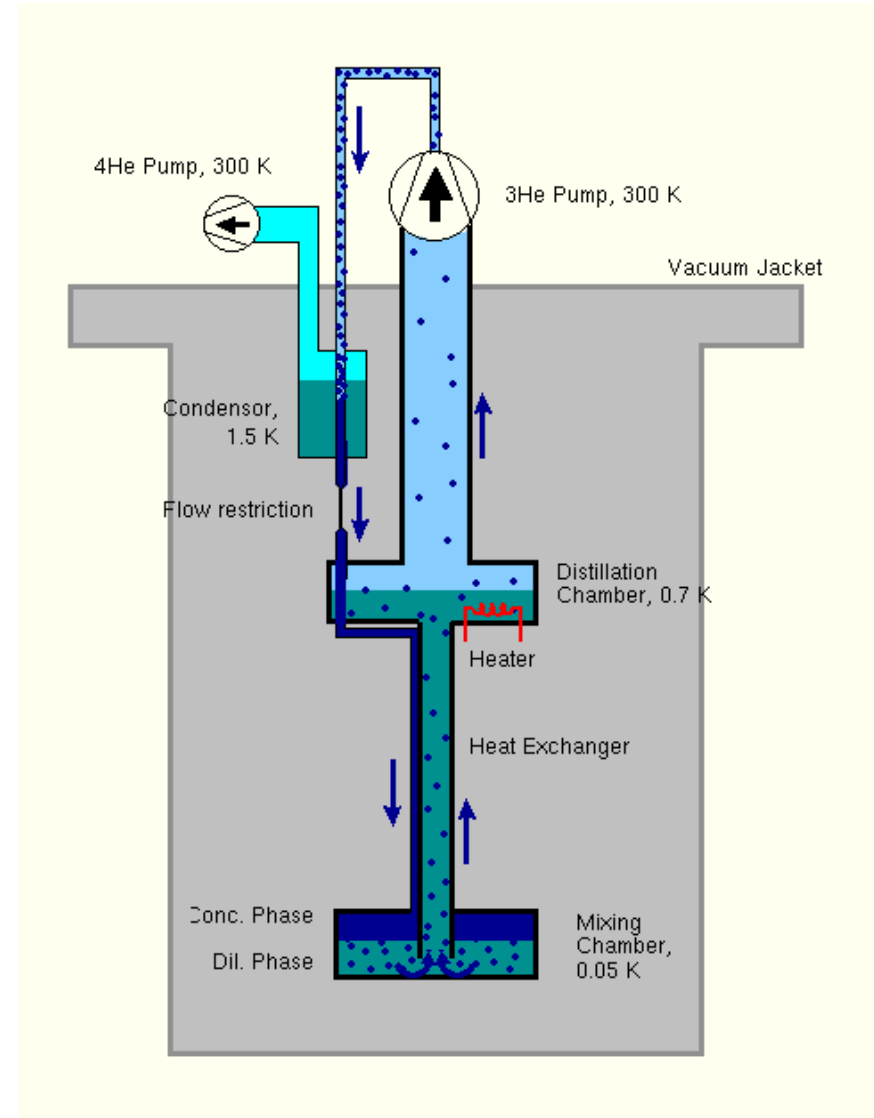
$$= n [94.5 T^2 - 12.5 T^2] = 82 n T^2 \quad \text{J/mol K}^2$$

Continuous Dilution Refrigeration

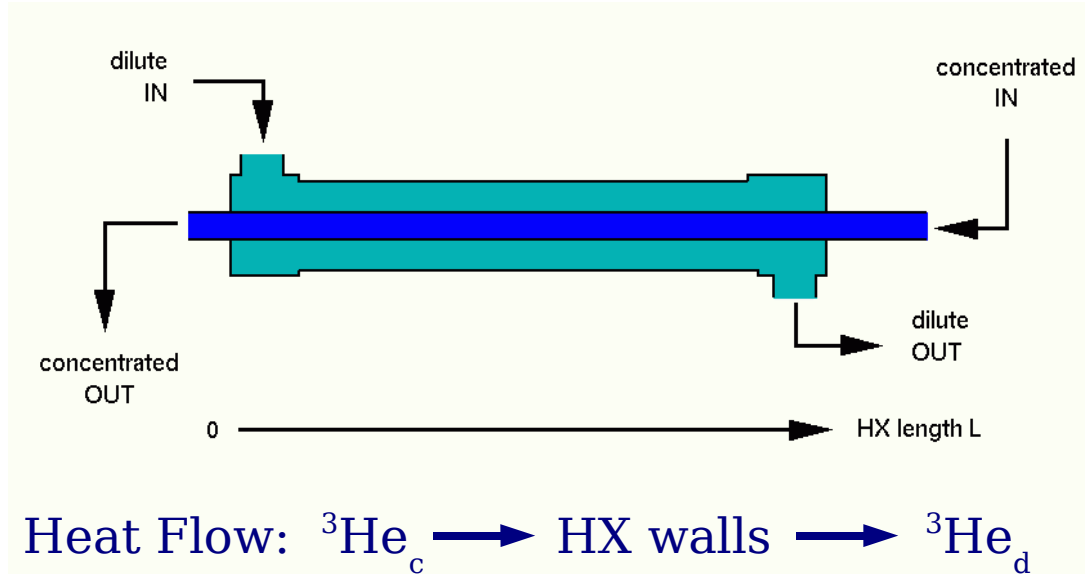
- ^3He is “distilled” from the lower, dilute phase of the mixing chamber
- after distillation, the ^3He is recondensed in a LHe bath at $\sim 1.5\text{K}$ and returned to mixer at elevated temperature T_c
- the cooling power and min. temperature depend strongly on heat exchange between the conc. (warm) and dil. (cold) fluid streams

$$\begin{aligned}\dot{Q}(T_m) &= \dot{n}[H_d(T_m^2) - H_c(T_c^2)] \\ &= \dot{n}[94.5T_m^2 - 12.5T_c^2]\end{aligned}$$

Performance of HX determines T_c



Heat Exchange between Concentrated and Dilute Phases



At low temperatures, the main impediment to heat transfer is the thermal boundary (Kapitza) resistance R_k between the helium and the HX walls

Only a small fraction of phonons from liquid will enter the HX walls

$$\frac{\rho_1 V_1^3}{\rho_2 V_2^3} \propto 10^{-5} \longrightarrow \dot{Q}_k = \frac{A}{2R_k} [T_2^4 - T_1^4]$$

Or a more familiar form: $\dot{Q}_k = \frac{\Delta T}{R} = \frac{AT^3}{R_k} \Delta T$ Heat transfer drops fast at low T !

Performance of an “Ideal” Heat Exchanger

(Giorgio Frossati, 1986)

$$\text{dilute side} \quad s_d \frac{d}{dx} \left[\kappa_d(T) \frac{dT_d}{dx} \right] + \eta_d \dot{V}_d^2 \frac{dZ_d}{dx} + \frac{dA}{dx} \frac{(T_c^4 - T_d^4)}{4R_{kT}} = \dot{n} C_d \frac{dT_d}{dx}$$

$$C_d \sim 107 \cdot T \text{ J/K}$$

$$\text{conc. side} \quad s_c \frac{d}{dx} \left[\kappa_c(T) \frac{dT_c}{dx} \right] + \eta_c \dot{V}_c^2 \frac{dZ_c}{dx} + \frac{dA}{dx} \frac{(T_c^4 - T_d^4)}{4R_{kT}} = -\dot{n} C_c \frac{dT_d}{dx}$$

$$C_c \sim 25 \cdot T \text{ J/K}$$

Axial conduction

s = sectional area
 κ = thermal cond.

Frictional heat

η = viscosity
 Z = flow impedance
 V = molar volume

Kapitza conduction

A = HX area (mean)
 R_{kT} = total Kap. resistivity

Enthalpy change

C = specific heat

Frossati: design HX so that 1st and 2nd terms are small compared to the 3rd

$$T_c^2 = \frac{2 \cdot 25}{(1 - (25/107)^2)} \frac{R_{kT}}{A} \dot{n} \approx 50 \frac{R_{kT}}{A} \dot{n}$$

Temperature of $^3\text{He}_c$
 entering mixing chamber

Cooling Power with Ideal Heat Exchanger

(Giorgio Frossati, 1986)

Cooling power, assuming “ideal” heat exchange is determined by molar flow rate and R_k/A of heat exchanger

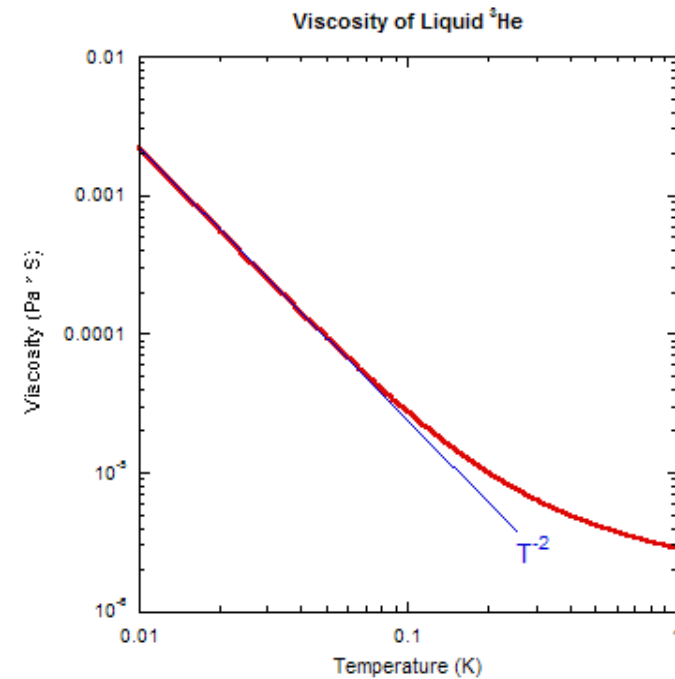
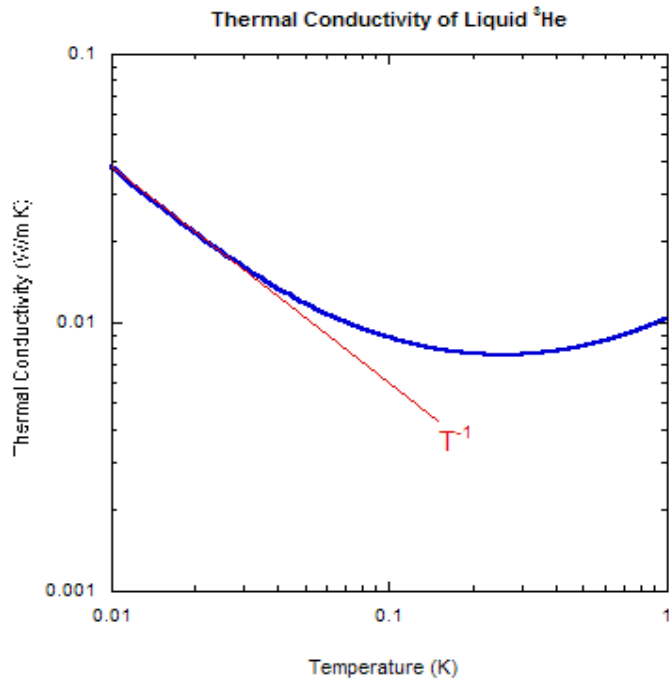
$$\begin{aligned}\dot{Q}(T_m) &= \dot{n} [94.5T_m^2 - 12.5T_c^2] \\ &= \dot{n} [94.5T_m^2 - 625 \frac{R_{kT}}{A} \dot{n}]\end{aligned}$$



Build HX with low R_{kT}
OR, large Area

Optimization of Heat Exchanger Geometry

To optimize heat exchangers, must consider heat leaks due to both axial conduction and frictional heating



$$Q_{cond} = \frac{\pi D^2}{4L} \int \kappa(T) dT$$

$$= aD^2$$

$$Q_{fric} = \eta \left(\frac{128L}{\pi D^4} \right) (\dot{n}V)^2$$

$$= bD^{-4}$$

Minimize $Q_{con} + Q_{fric}$: $\frac{d}{dD} (aD^2 + bD^{-4}) = 0 \quad \longrightarrow \quad \underline{D_{opt} = (2b/a)^{1/6}}$

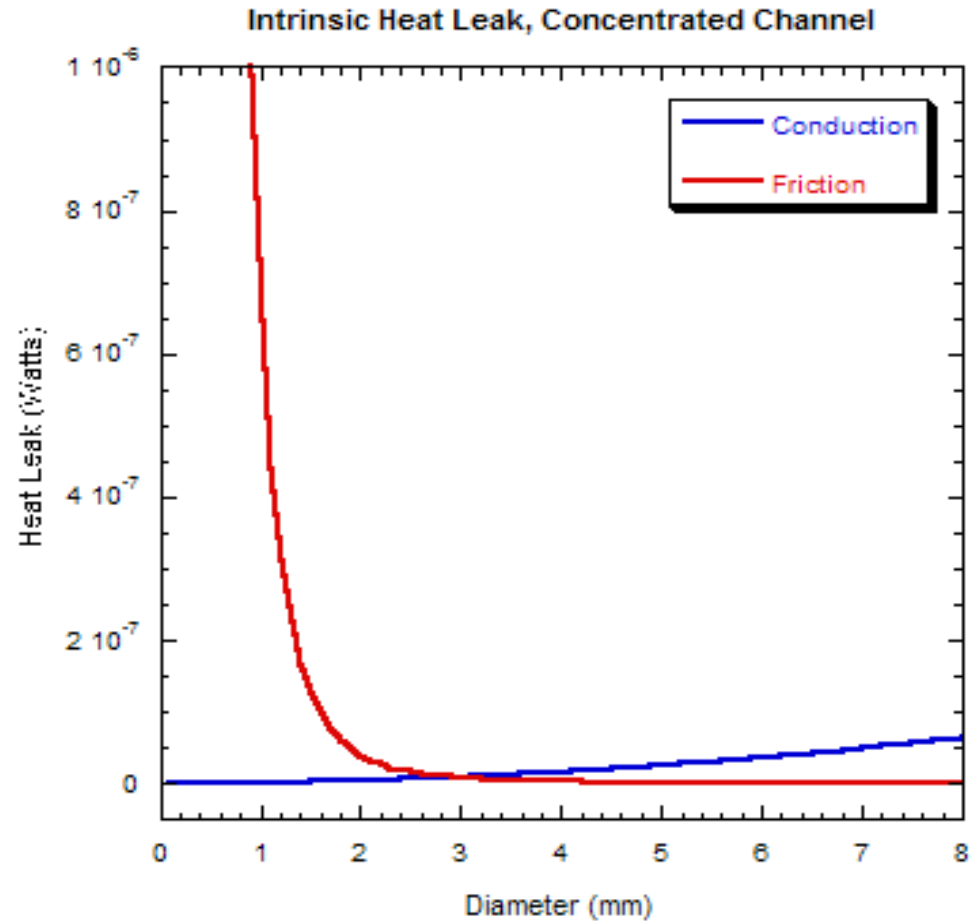
Intrinsic heat leak as a function of tube diameter

HX Length: 1.5 m

Flow rate: 1 mmol/s

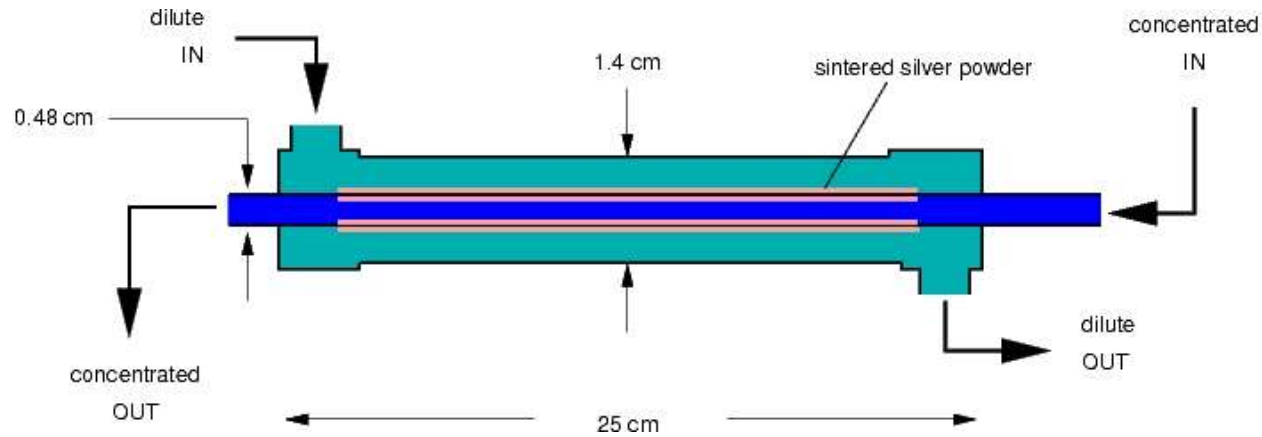
Inlet temperature: 200 mK

Outlet temperature: 20 mK

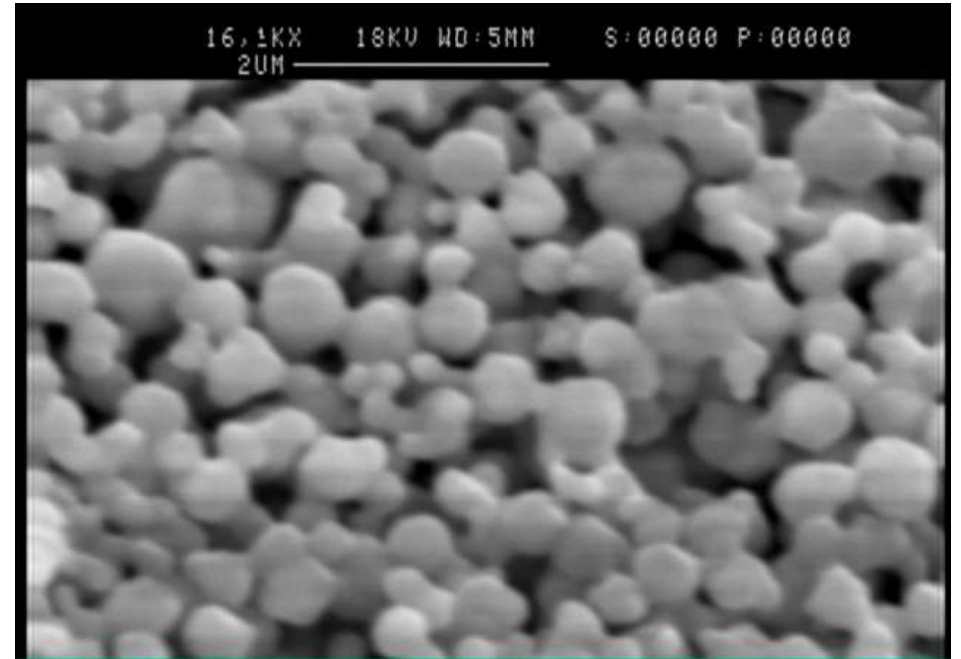


Sintered Silver Heat Exchangers

- large surface areas are necessary to overcome Kapitza resistance
- use sinters of ultra-fine silver powder to provide several m^2 of area



JLab: Use 5 identical segments (in series) between Still and Mixer



1 micron Ag powder

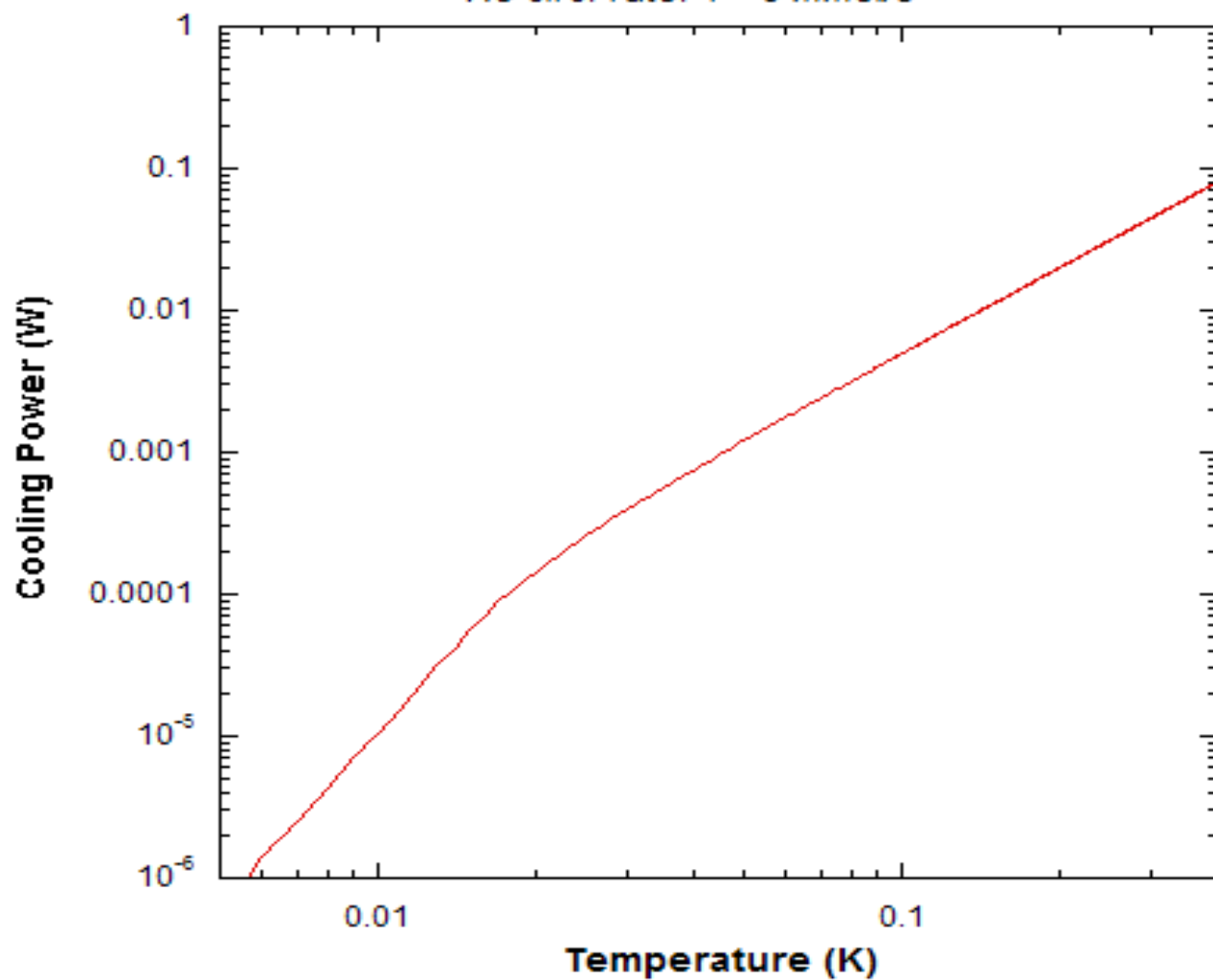
Sinter at 250 °C → 0.5 m²/g

each segment: Dil. = 15 g = 7.5 m²
Conc. = 8.5 g = 4.2 m²

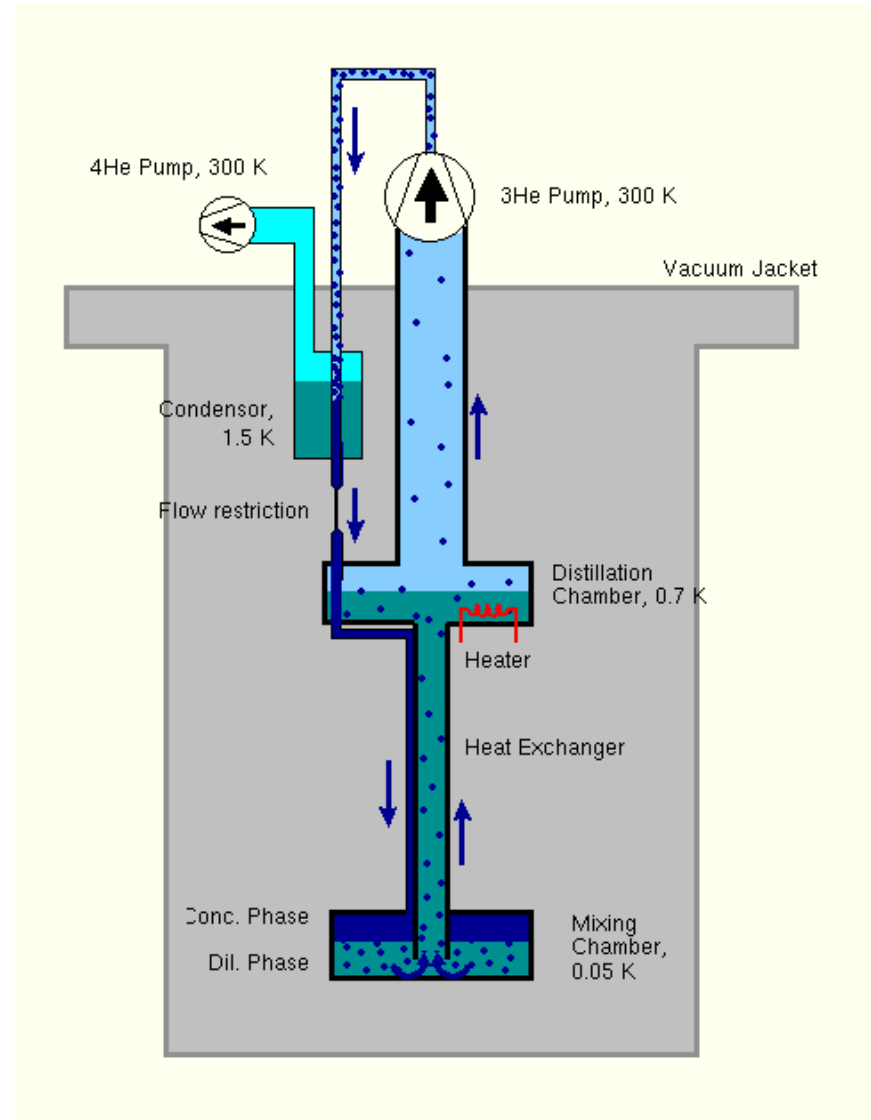
5 segments: Dil. = 37.5 m²
Conc. = 21 m²

CoolingPower, "Ideal" Heat Exchanger

³He circ. rate: 1 - 6 mmol/s



An example of a commercial, vertical dilution refrigerator

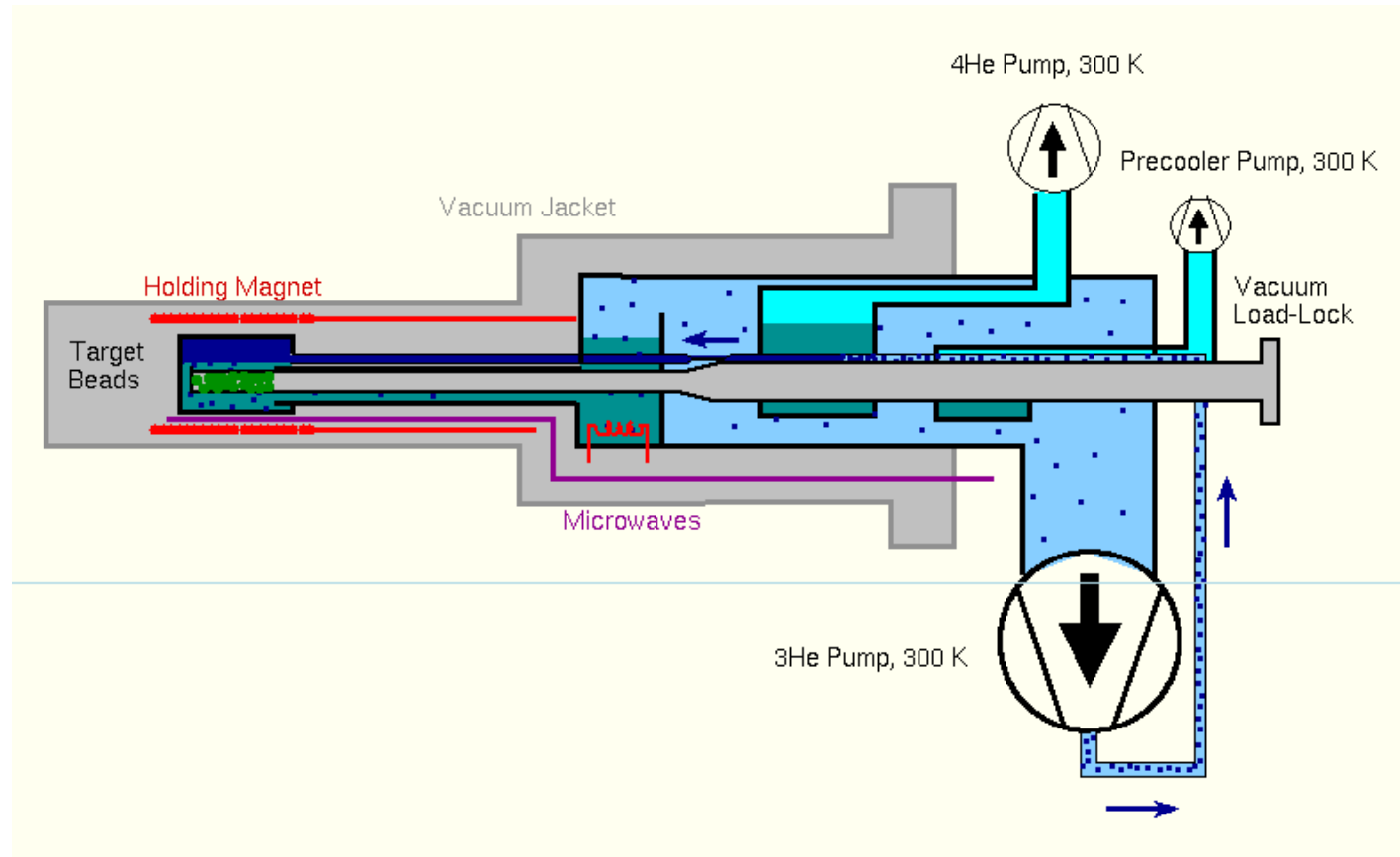


© *Leiden Cryogenics, BV*

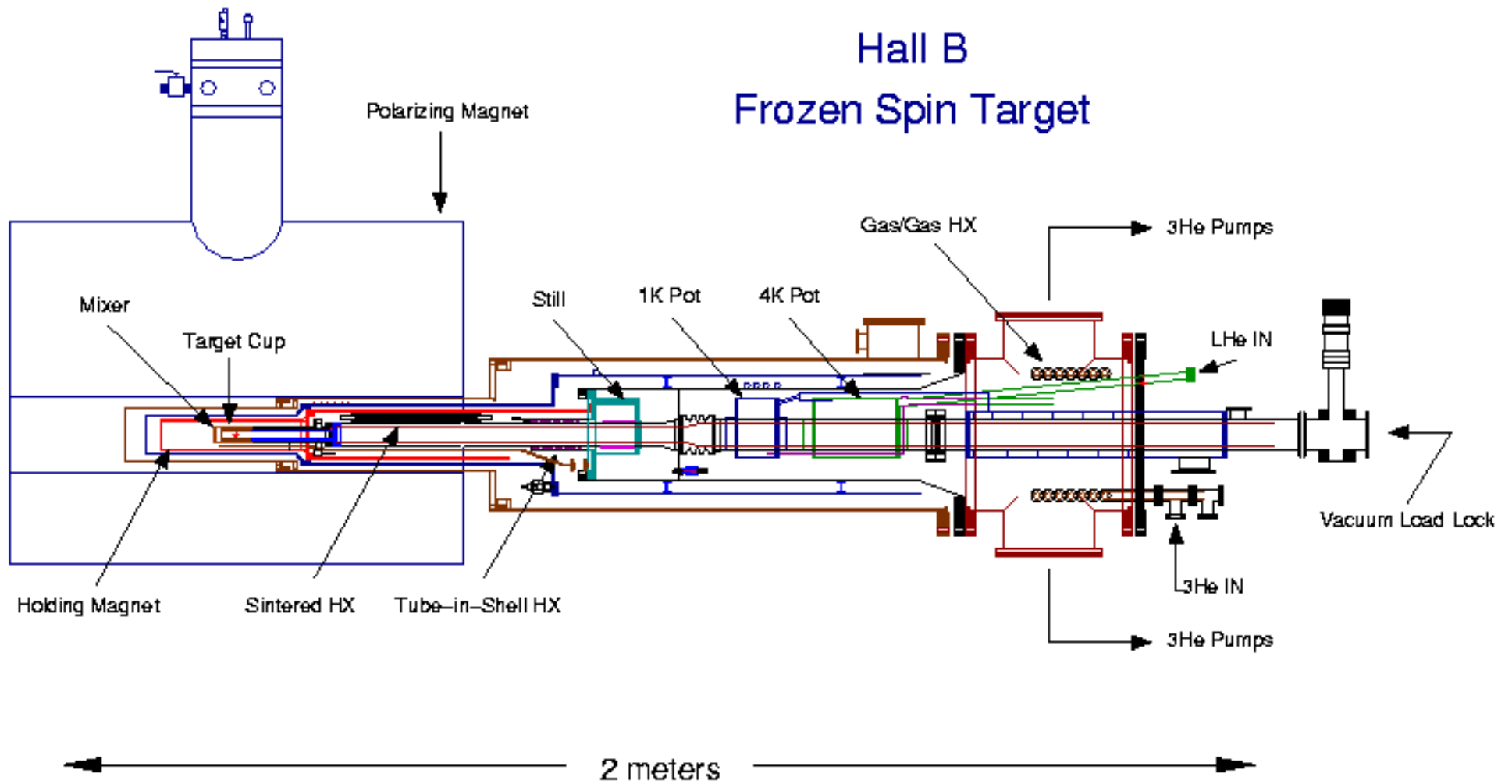
Very nice, but it won't fit inside CLAS...

Horizontal Dilution Refrigerator for Frozen Spin Target

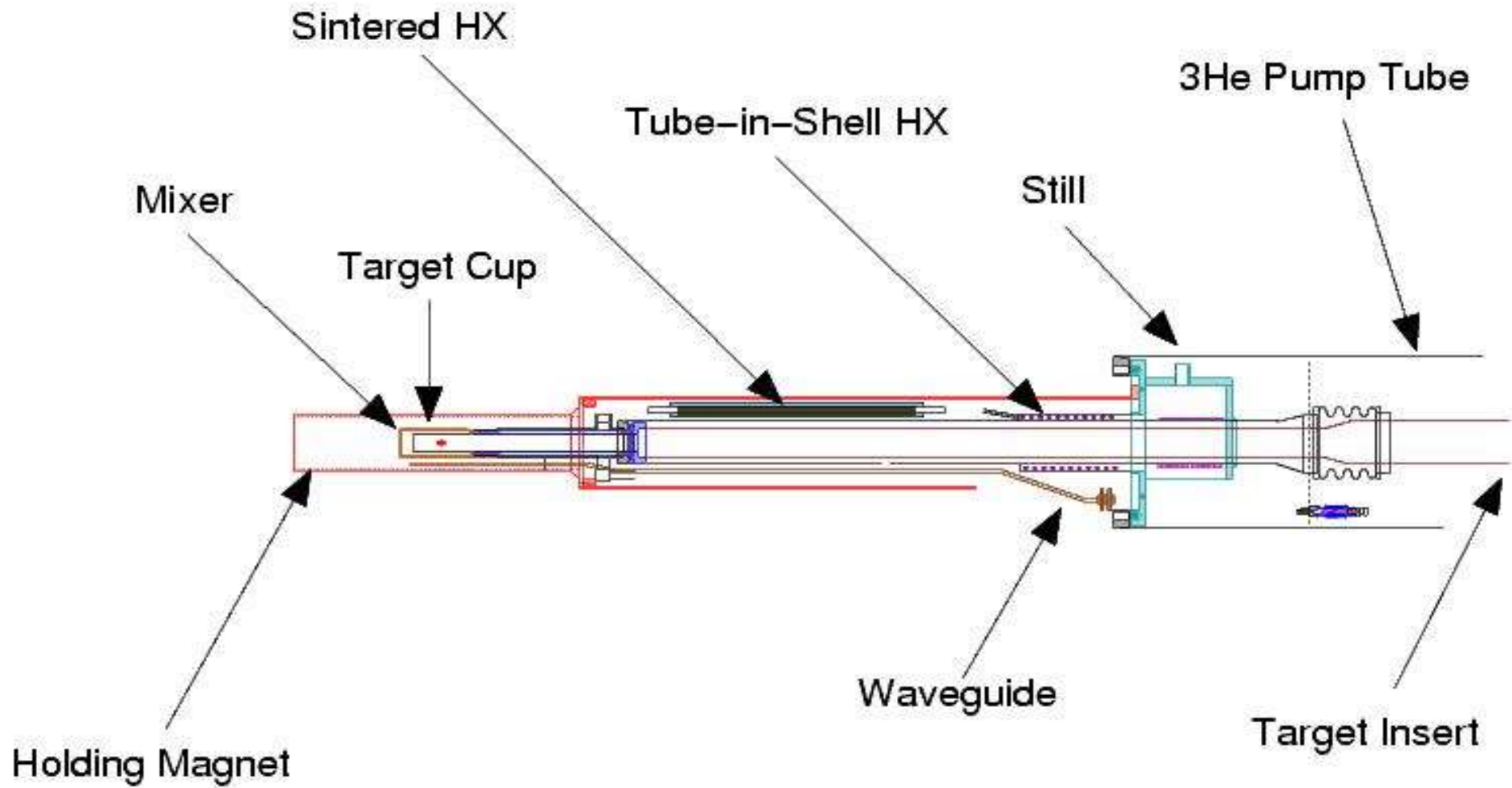
T.O. Niinikoski, CERN 1971



Hall B Frozen Spin Target



Dilution Unit



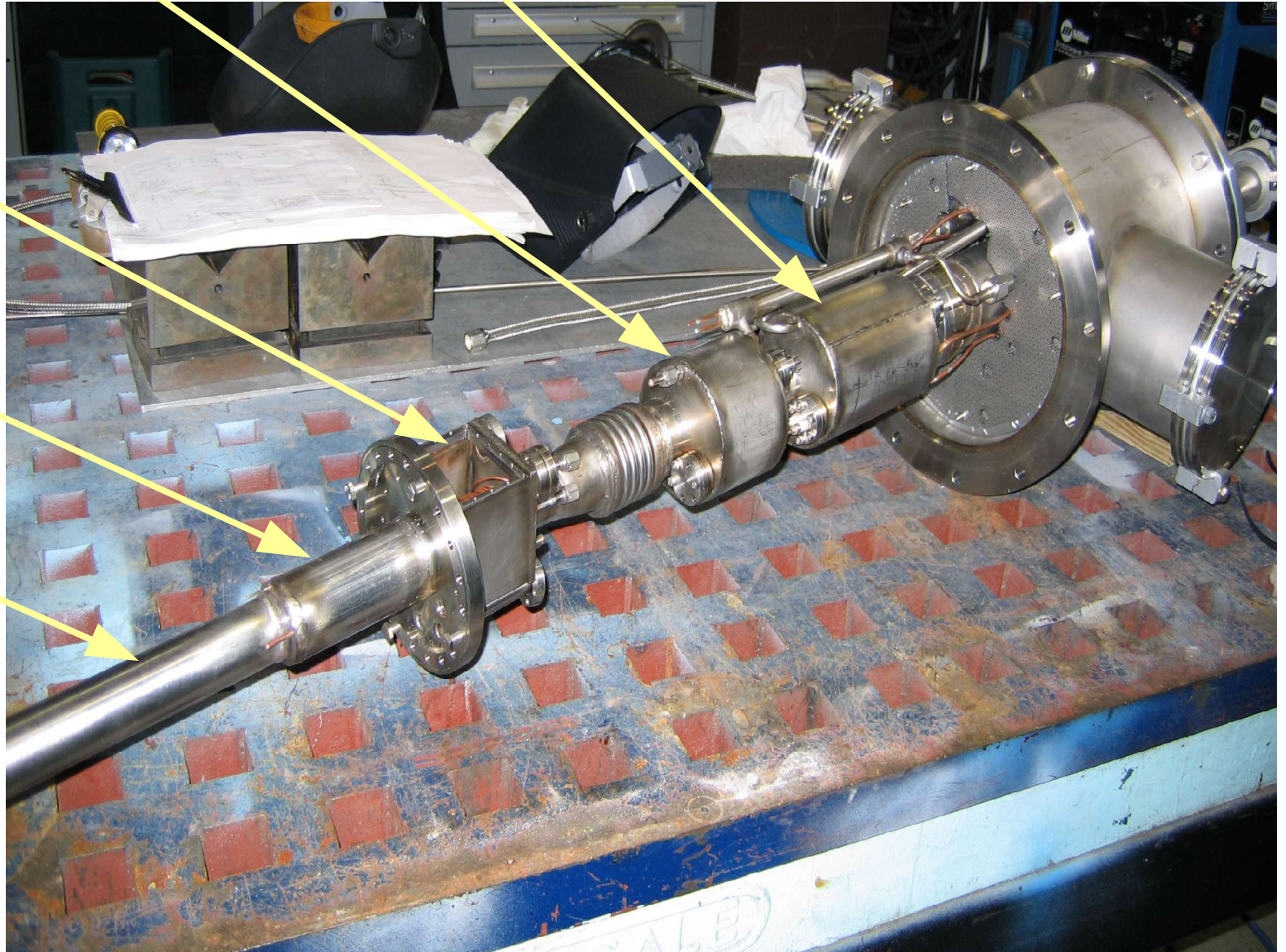
1K Pot

4K Pot

Still

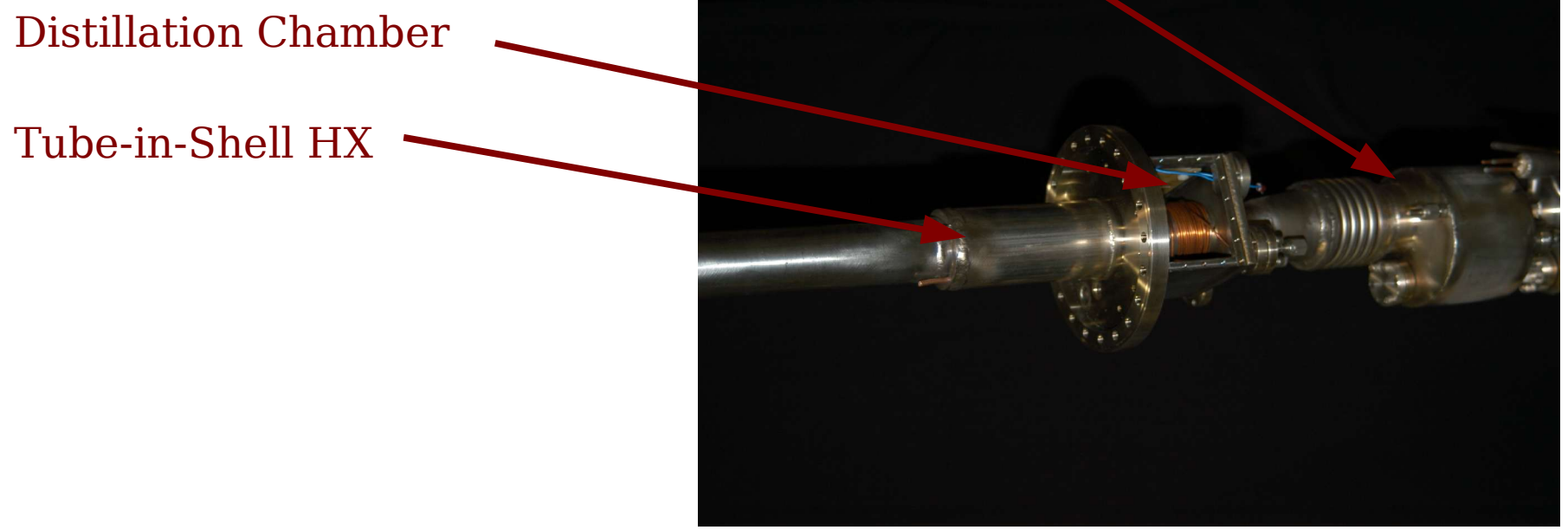
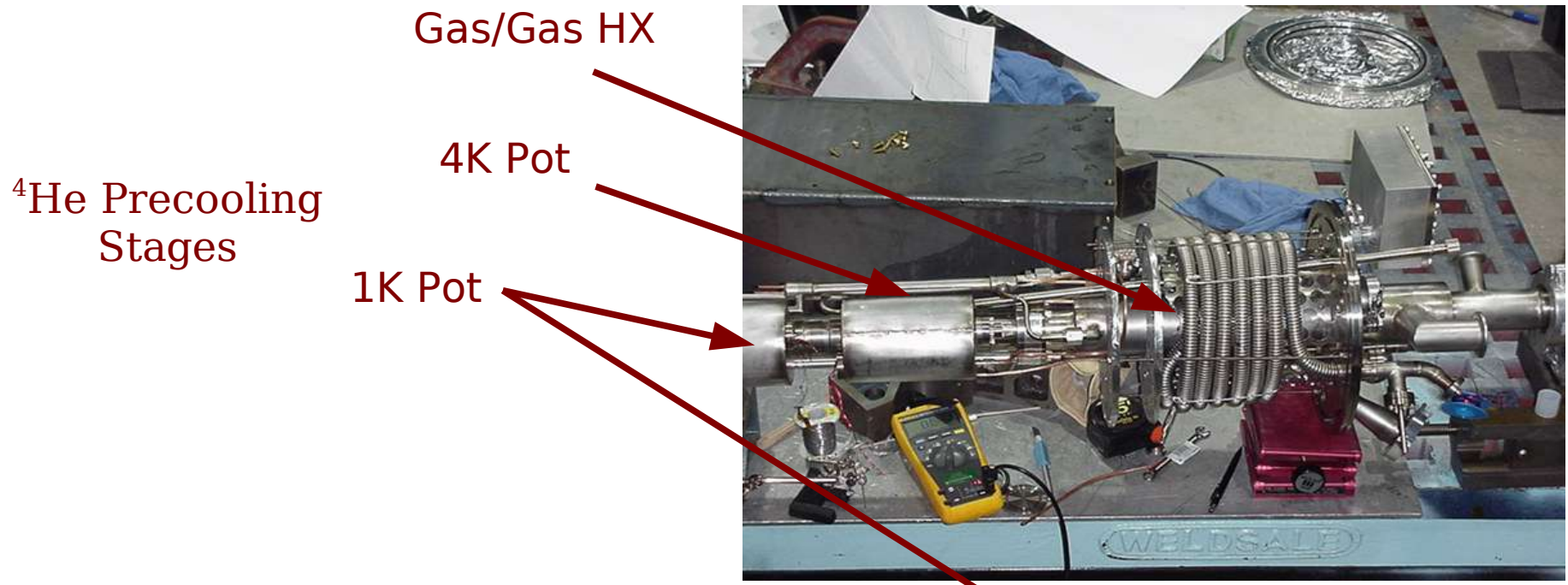
Tube-in-Shell HX

Vacuum Load Lock



Outer Vacuum Jacket

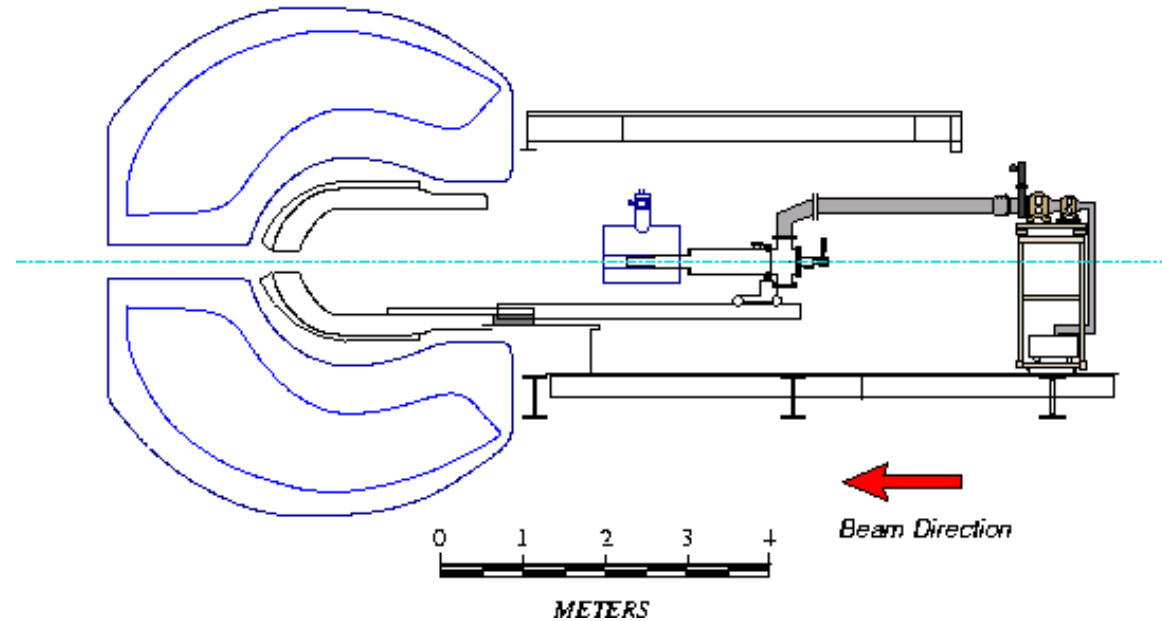




The Frozen Spin Waltz

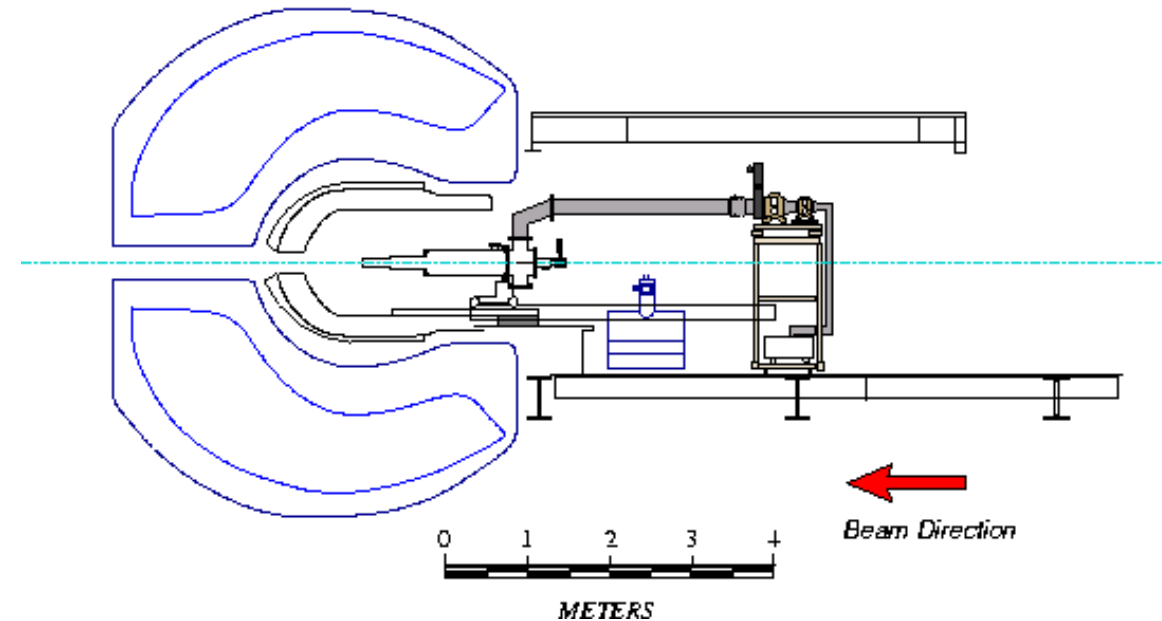
Step 1: Polarizing

- Target is fully retracted, magnet is lifted to beam height
- Target is inserted into magnet, magnet energized, microwaves on



Step 2: Beam On

- Microwaves off, magnet off, holding coil on
- Target is fully retracted, magnet is lowered
- Target is fully inserted into CLAS



Summary

- A frozen spin polarized target for tagged photon experiments is under development at Jefferson Lab.
- 5 Tesla polarizing magnet is in house.
- Superconducting holding coils (~ 1 mm thick) are under development.
 - longitudinal solenoid (0.4 Tesla) constructed and tested
 - prototype of transverse dipole has been tested (0.3 Tesla)
- Horizontal dilution refrigerator is under construction.
- Positioning system for Hall B is still in conceptual design stage.